

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
14 August 2003 (14.08.2003)

PCT

(10) International Publication Number  
WO 03/067510 A1

(51) International Patent Classification: G06K 7/10,  
H01S 3/13, 3/00

(21) International Application Number: PCT/US03/01032

(22) International Filing Date: 14 January 2003 (14.01.2003)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
60/348,967 14 January 2002 (14.01.2002) US

(63) Related by continuation (CON) or continuation-in-part (CIP) to earlier applications:  
US 09/724,692 (CIP)  
Filed on 28 November 2000 (28.11.2000)  
US 60/348,967 (CIP)  
Filed on 14 January 2002 (14.01.2002)

(71) Applicant (for all designated States except US): CEYX  
TECHNOLOGIES, INC. [US/US]; 437 J Street, Suite  
311, San Diego, CA 92101 (US).

(71) Applicant and

(72) Inventor: SANCHEZ OLEA, Jorge [US/US]; 15655  
Oakstand Road, Poway, CA 92064 (US).

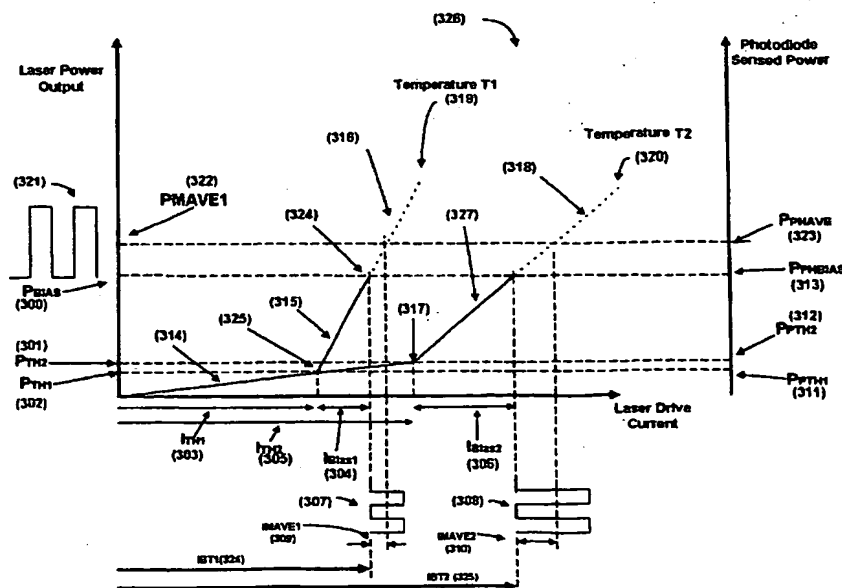
(74) Agent: PARSONS, George, T.; 2736 Aegean Drive, San  
Diego, CA 92139-3211 (US).

(81) Designated States (national): AE, AG, AL, AM, AT, AU,  
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,  
CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH,  
GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC,  
LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,  
MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG,  
SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VN,  
YU, ZA, ZM, ZW.

(84) Designated States (regional): ARIPO patent (GH, GM,  
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW),  
Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM),  
European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE,  
ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, SE, SI,  
SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN,  
GQ, GW, ML, MR, NE, SN, TD, TG).

[Continued on next page]

(54) Title: LASER TEMPERATURE PERFORMANCE COMPENSATION



(57) Abstract: The invention presents a method that calibrates the laser optical power (202) in a continuous manner without disrupting the flow of information in the optical communications link. The method utilizes knowledge of the measured value of the laser optical power(202) and makes necessary adjustments to optimize the values of the Extinction Ratio, Bit Error Rate and to compensate for aging. The method utilizes knowledge of the temperature from a sensor (114) and mathematical models, which contain parameters which are updated for a specific laser configuration.

WO 03/067510 A1

**Declaration under Rule 4.17:**

- of inventorship (Rule 4.17(iv)) for US only

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*

**Published:**

- with international search report
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments

## **LASER TEMPERATURE PERFORMANCE COMPENSATION**

### **Reference to other applications**

This application is a continuation in part application for co-pending US patent application serial number 09/724,692 filed on November 28, 2000, titled "Electro-  
5 Optic System Controller and Method of Operation". This utility application is also filed based on provisional application 60/348,967 filed January 14, 2002, entitled "Laser Power Sensing Methods."

## **BACKGROUND**

### **Field of the Invention**

The invention relates to a set of methods used to compensate the performance of lasers given changes with temperature. Precise sensing of laser power magnitudes is obtained with the use of temperature sensors and slow photodiodes and without any  
15 disruption of data transmission.

### **Description of the Related Art**

A substantial number of lasers are monitored with the use of photodiodes that are integrated with the laser in the same package or that are part of an integrated circuit that is associated with the driver or a VCSEL laser array. In addition, temperature  
20 sensors are utilized to determine when adjustments are appropriate. There is a significant demand in the industry to understand and control the magnitude of the optical power in order to perform adjustments to the laser driver to stabilize the extinction ratio and reduce the Bit Error Rate (BER).

### **Unresolved problems related to sensing laser power.**

It is common to utilize very slow photodiodes for monitoring the laser output. In some cases the photodiodes exhibit a frequency response that is several orders of magnitude lower than the frequency response of the laser. This type of performance poses a problem in determining the amplitude of the optical pulses for transmitting  
30 information since in some cases the photodiode will not generate significant output in response to the ac power output representing the data transmission. In digital communications, the amplitude of the optical pulses is necessary in order to distinguish the transmission of a logical one from the transmission of a logical zero.

In both analog and digital communications, the magnitude of the optical signal represents the strength of the signal and has a direct impact on signal to noise ratio and transmission reliability.

5 Sensing the power with slow photodiodes poses a problem because only the average power of the laser is sensed due to the low frequency response of the photodiode. This situation prevents the laser control system from determining the amplitude of the data transmission light pulses. Thus, adequate feedback information will not be available to adjust the magnitude of optical pulses representing the data. The optical output  
10 will not be properly controlled and the Extinction Ratio and Bit Error Rate (BER) will change with temperature and well as with aging.

### SUMMARY OF THE INVENTION

15 The method in this invention calibrates and stabilizes the bias and modulation currents. The threshold needed to turn on the laser is determined and a minimum DC bias current is chosen above the threshold. A value for the temperature drift model of the threshold current is determined and the value is stored in the Digital Controller (111) memory. Temperature coefficients for other parameters are stored in the  
20 Digital Controller (111). Once the system is in the field, the control system utilizes the photodiode sensor to continuously adjust the value of the average laser current to a fixed value above the minimum laser threshold. With the use of various algorithms, the value of the optical power corresponding to the logic one is adjusted to maximize signal transmission reliability.

### BRIEF DESCRIPTION OF THE DRAWINGS

Details of the invention, and of the preferred embodiment thereof, will be further understood upon reference to the drawings:

30 **FIG 1** illustrates a control system diagram for a laser transmitter;  
**FIG 2** illustrates the timing diagram for the calibration process; and  
**FIG 3** illustrates graphically the calibration method.

## DETAILED DESCRIPTION OF AN EMBODIMENT

The above-mentioned unresolved problems related to laser sensing power are overcome by the present invention.

5

**FIG 1** shows a block diagram for a Laser Control System (114). The system consists of a drive Signal Input (100) applied to a Laser Module Driver (101), which contains a Bias Current Generator (102) and a Modulation Current Generator (103). The current generators are controlled by Bias Control Signal (112) and Modulation Control Signal (113). The Driver (101) produces Modulation Current (104) and Bias Current (105), which are applied to the Laser Module (106). The Laser Module (106) in turn produces Light Output (107). The magnitude of the Light Output (107) bears a relationship to the magnitude of the Modulation Current (104) and the Bias Current (105). A portion of the Light Output (107) from the laser is sensed. This constitutes the Optical Power Sense (108), which is coupled to a Photodiode Sensor (109). The Photodiode Sensor Output (110) is connected to a Digital Controller (111). In addition, a temperature sensor (114) provides temperature information to the Digital Controller (111). The Digital Controller (111) contains algorithms for laser control and also determines the magnitudes of the Bias Current Generator (102) and Modulation Current (103).

20

**FIG 2** shows the timing of the calibration of the laser optical power. As a reference to the timing of the system, a system clock CLK (200) is utilized by a transponder. The transponder is an optical communications transceiver with interface to a parallel computer bus. The clock (200) is utilized in the system to generate Serial Data Di (201). In this example the Serial Data Di (201) consists of a sequence 101. The data transmission of the timing diagram in the illustration corresponds to NRZ-L. After the zero to one transition of the Serial Data Di at (205), the data flows through the Driver (103) and causes a zero to one transition in Laser Optical Power Output  $P_L$  (202). This transition of the Laser Optical Power (202) happens after a delay  $t_{Drive}$  (206), corresponding to the delay of the signal flowing through the Driver (103) and the Laser (106). A given setting of the Bias Current Generator (102) places the Laser (106) at a value above the threshold. This setting can be adjusted and controlled

25

30

independently from the signal modulation current. For the purpose of calibrating the Light Output (107), the control of the Laser Bias Current Generator (102) is used. Corresponding to the pulse of the Serial Data  $D_i$  (201), there is an amplitude of the Laser Optical Power Output  $P_L$  (202). The magnitude of the Optical Power Output (202) is noted as  $PL_{max}$  (210). The laser optical power corresponding to the transmission of a logical 1 will vary depending on the setting of the Modulation Current Generator (103), the Laser (106) characteristics and the effects of factors such as temperature and aging on the Laser (106). The magnitude of the laser power output corresponding to a transmission of a logical zero is  $PL_{min}$  (212). This power output corresponds to the power generated from the application of the bias current from the Bias Current Generator (102). Light from the laser is sensed by the Photodiode (109). There may be a sample and hold device inserted between the photodiode sensor and the analog to digital converter that is part of the controller (111). There is generally an amplifier connected to the photodiode output that is used to amplify the photodiode signal. The photodiode amplifier will generate a voltage output corresponding to the optical power sensed by the photodiode (109). Since the Photodiode (109) is relative slow, the sensing circuit will exhibit a Photodiode response, which corresponds to an average photodiode response VPS (203) of the laser power received by the photodiode. The steady value of the photodiode response integrates the value of the laser optical power output (202). In the example illustrated in FIG 2, the Serial Data (210) is assumed to be so fast, that the photodiode senses only the average of a laser optical power pulse. The zero photodiode current VPZ (209) is the Photodiode response with no applied laser power and may correspond to a photodiode dark current. This current can be subtracted from all measurements to further preserve accuracy with temperature changes. As is discussed below, one need to rely only on the average current to control and stabilize the laser output.

In FIG 3, the Laser Power Sensing Method is illustrated.

The characteristic 319 corresponds to the overall laser response at temperature T1.

The characteristic is comprised of several piecewise linear sections. The first section 314 is the region before the laser threshold is reached; the second region. The second region 315 corresponds to the combined transfer characteristic of the bias current source and the laser beyond threshold. The third region 316 corresponds to the

combined transfer characteristic of the modulation current source and the laser beyond threshold. Since the bias and modulation current are summed together, using the superposition principle, we can graphically represent the overall transfer characteristic by stacking 316 on top of 315. The origin of 316 is at the bias set point (324). This characteristic exhibits a threshold current of ITH1 (303). Corresponding to this particular threshold, there is a laser power output PTH1 (302) and a sensed photodiode power PPTH1 (311) by the photodiode detector. In this example a laser bias current IBIAS1 (304) with a value above the threshold is shown. The bias current produces a corresponding optical power output from the laser PBIAS (300). A portion of the laser optical power output is sensed by the photodiode resulting in a photodiode output PPBIAS (313). Data transmission is accomplished by applying a modulation current to the laser represented by a square wave (307). The power output is represented by the square wave (321). The above parameter values are determined during the factory calibration of the laser and photodiode.

#### **Calibration process adjustments at a first temperature T1.**

The following calibration process for Bias and Gain are is carried out in the laser transmitter factory. The temperature at the factory is referred to as T1.

1. Threshold current ITH1 (303) is obtained at power up with an algorithm that uses the photodiode to find the threshold by monitoring the slope of the laser characteristic. The modulation current (307) is turned off while the system searches for the threshold. When the slope changes, the threshold is found. Obtaining the threshold may require averaging of the monitored signal to account for noise in the system. A signal-processing algorithm with a digital filter may also be used.
2. Additional Bias current IBIAS1 (304) is applied as required by the specific design of the system. We thus set the Bias Current Generator (102) to produce a Total Bias Current  $I = IBT1 (324) = ITH1 (303) + IBIAS1 (304)$ . During the factory calibration, the photodiode sensor (109) and the temperature sensor (114) sense the power and temperature. Values are recorded in order to calibrate the measurement. At the same time, actual laser power is determined with an external Optical Power Meter connected to the output of the laser.

3. Laser power PTH1 is obtained from the value given by the Optical Power Meter. The value of the photodiode current PPTH1 (311) is measured and an Optical Power Meter determines the light output (107) from the laser.
4. Above data provides two sets of data points 324, 325, which are used to obtain the slope GB1 of the laser characteristic in section 315 at temperature T1.
5. A scaling factor K for the photodiode sensor is determined using the two sets of photodiode values obtained PPTH1 (311) and PPTH2 (312) corresponding to the actual values ready by the Optical Power Meter PTH1 (302) and PTH2 (301). Photodiode transfer characteristic is assumed to be linear.
6. Set the total bias current to IBT1 (324)
7. Apply a modulation current (307). This current is generated by a second current source and is added to the bias current. The modulation current is of a necessary average value IMAVE1 (309). This modulation current can be obtained either by using a steady DC modulation current value IMAVE1 (309) or by a suitable train of square waves (307). IMAVE1 (309) is modified until the required value of PMAVE1 (322), which is needed for the transceiver is obtained. As before, an Optical Power Meter is used to determine a calibrated value of the power.
8. The corresponding value of the photodiode sensor (109) reading is recorded for calibration purposes
9. Compute the slope GM1 of the laser characteristic in section 316 at temperature T1
10. Parameters for model of temperature drift of the threshold current for the laser are entered in the Digital Controller (111).
11. The temperature coefficients TCOGB and TCOGM corresponding to the slope for the Bias (GB) and Modulation (GM) slope are stored in the Digital Controller (111).

#### **Calibration adjustments at a second temperature T2.**

All adjustments after the factory calibration and after the power up sequence of the laser transmitter are used to account for temperature changes and are made on a continuous basis and without interrupting the transmission of information. Because



the adjustments are made on a continuous basis, the extinction ratio is preserved and BER is minimized.

Temperature of the laser is constantly monitored and at the appropriate temperature change a calibration control process is executed. For the purpose of maintaining calibration at temperature T2, the threshold ITH2 (305) is determined with a mathematical model of the threshold current change with temperature (drift). This model can be a table of values of the threshold current for temperature data points, a coefficient for the drift or an equation. For example, in VCSEL (Vertical Cavity Surface Emitting Laser) lasers this drift can be modeled with an equation where the threshold current versus temperature characteristic exhibits a quadratic relationship about an initial value.

The portion of the characteristic before the threshold (314) can be approximated with a straight line using a piecewise linearity method. With this method, a line extends from the origin to the data point 325 with coordinate values of ITH1 (304) and PTH1 (302). The threshold drift model yields the value of PPTH2 (312) and the laser power output PTH2 (301). We can assume that the photodiode transfer characteristic drift will have a negligible error due to temperature changes although a model can be incorporated into the system to account for temperature drift.

The following list shows the process for performing adjustments to compensate for the temperature change to an arbitrary value of T2.

**Calibration at temperature T2.** In this process, it is assumed that the transceiver is installed and is sending data at a steady rate.

1. An updated value of the threshold current ITH2 (305) at the new temperature T2 is obtained from the temperature drift model of the laser threshold current.
2. An updated value of the Bias current IBIAS2 (306) at the new temperature T2 is obtained using the temperature coefficient for the laser bias current.
3. The total bias current IBT2 (324) = ITH2 (305) + IBIAS2 (306) at the new temperature T2 is determined and then applied by adjusting the bias current generator (102) with the new value.
4. The Modulation current IMAVE2 (310) at the new temperature is determined using the temperature coefficient of the modulation (TCOGM). This value of

IMAVE2 (310) is such that the light output (107) is preserved to a value of PMAVE1 (322). The Modulations current generator (103) is adjusted to produce the new value of IMAVE2 (310).

5 The previous embodiment uses temperature for feedback to the control system. Alternative embodiments also use the average power sensed by the photodiode PPHMAVE (323) to adjust the modulation current.

In this case, a measurement is done by averaging the signal from the photodiode (109) over numerous cycles of the input Drive Signal (100). In digital data transmission,  
10 Commonly, data patterns are not allowed to become all 1's or all 0's. Thus long averaging of the light output (107) will result on a value of the power corresponding to approximately  $\frac{1}{2}$  the amplitude of the peak value of the power. Average power information is then used to set modulation current IMAVE2 (310) to the correct amount that yields the original value of the power PMAVE1 (322) at the prior  
15 temperature T1.

#### Extinction Ratio and Bit Error Rate Optimization.

Once the laser characteristic is calibrated at the new temperature T2 optimal value of extinction Ratio and minimal Bit Error Rate are obtained. The firmware imbedded in  
20 the Digital Controller (111) utilizes the results from the A/D conversion of the sensor and proceeds to make adjustments to the amplitude of the peak laser power in response to the logic high sent. The laser power for logic high needs to send a signal with a sufficiently large value according to the transmission protocol. With the precision power measurement circuit of this invention, the laser is not overdriven thus  
25 extending operating life.

The Digital controller (111) makes adjustments to the minimal optical power in response to the logic low sent and. The minimal optical power is determined by the Bias Current Generator (102) and is adjusted above the threshold of the laser. The  
30 current needs to strike a balance between having too low of a value (needed to maximize extinction ratio) or too high of a value (needed to obtain a margin over the lasing threshold and to not operate over the noisy region of the laser near the threshold). Since one can conduct the above adjustments on a continuous manner, the

laser is always operated at the optimal levels of power output.

Other embodiments of the algorithms described above can be applied as well to analog signal transmission or other laser applications.

5

While the foregoing description has described the principle and operation of the present invention in accordance with the provisions of the patent statutes, it should be understood that the invention may be practiced otherwise as illustrated and described above and that various changes in the size, shape, and materials, as well as on the details of the illustrated method of operation may be made, within the scope of the appended claims without departing from the spirit and scope of the invention.

10

What is claimed is:

15

1. A method to compensate for the effects of temperature on laser power in an optical transceiver, wherein the method is performed without disrupting communication comprising the steps of:

5 performing an initial factory calibration;  
updating the value of the Bias Current IBIAS2 (306) at the new temperature T2 using a temperature drift model;  
adjusting the bias current generator (102) with a new value;  
updating the value of the Modulation current IMAVE2 (310) at the new  
10 temperature T2 using a temperature drift model; and  
adjusting the bias current generator (102) with a new value.

2. A method to compensate for the effects of temperature on laser power in an optical transceiver as in claim 1, wherein the initial factory calibration  
15 further comprises the steps of:  
using a threshold finding algorithm;  
setting Total Bias IBT1 (324);  
setting Modulation current IMAVE1 (309) to obtain desired value;  
computing the slope GB1 and GM1 of the laser characteristic at temperature  
20 T1; and  
entering temperature coefficients for the laser characteristic slope in bias and modulation regions.

3. A method to compensate for the effects of temperature on laser power in an  
25 optical transceiver as in claim 1, wherein the information utilizes measured values to optimize Extinction Ratio and Bit Error Rate.

4. A method to compensate for the effects of temperature on laser power in an  
30 optical transceiver as in claim 1, wherein the information utilizes average photodiode information to compensate for laser aging.

5. A method to compensate for the effects of temperature on laser power in an optical transceiver as in claim 1, wherein thermal drift models are utilized to

determine the magnitude of the modulation power without measuring the power with the photodiode.

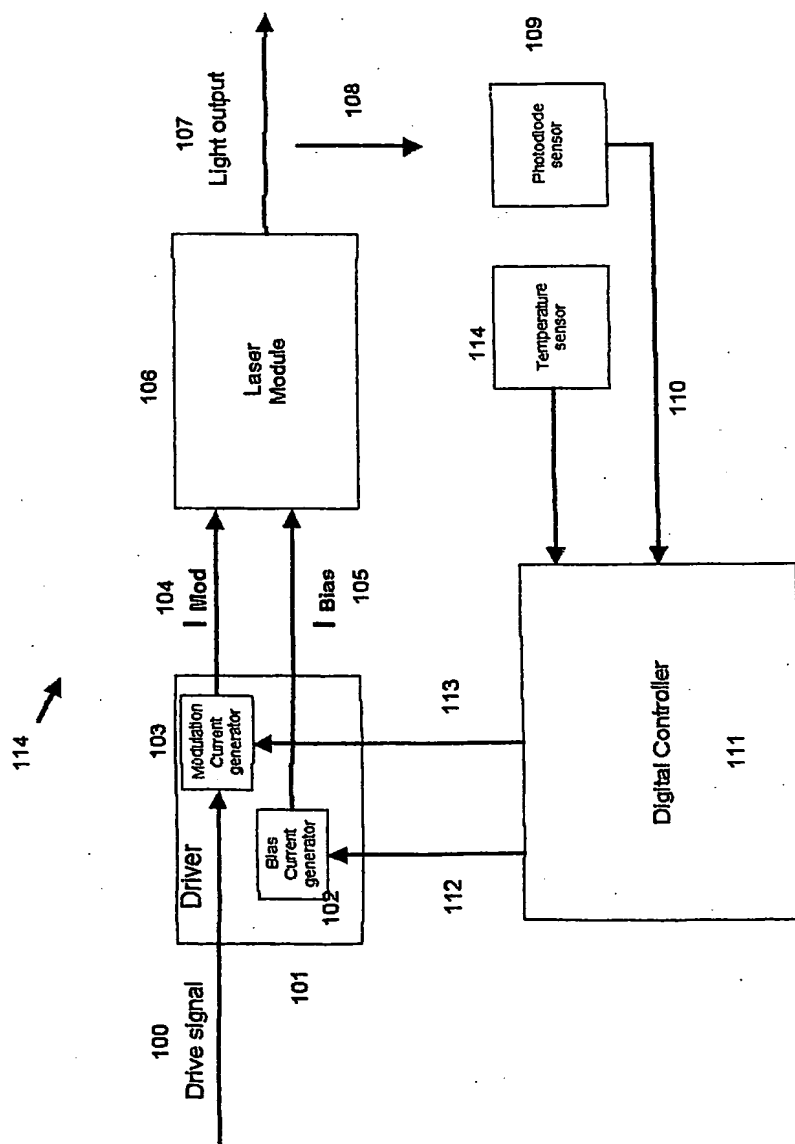


Figure 1.  
Control system block diagram

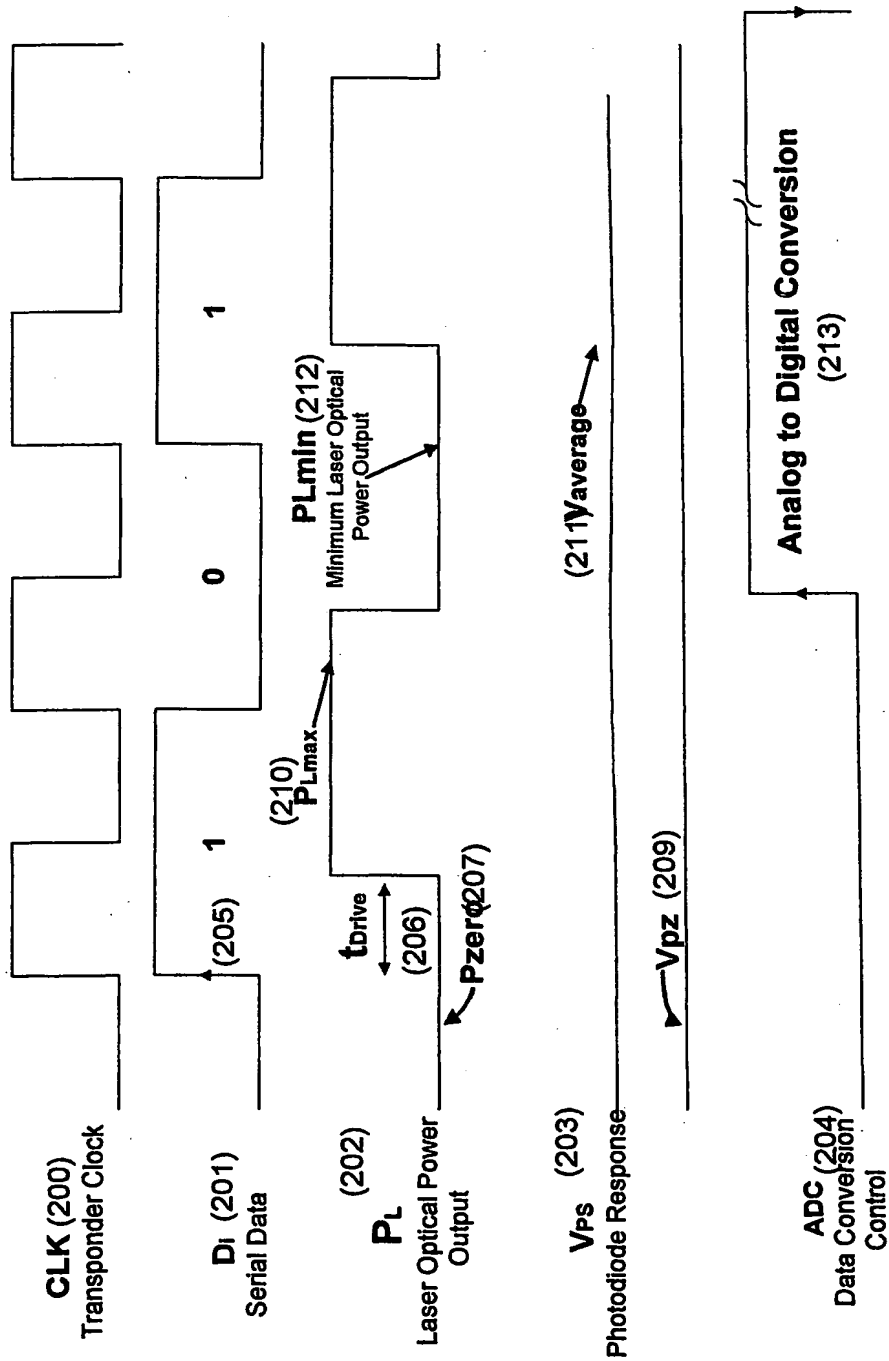
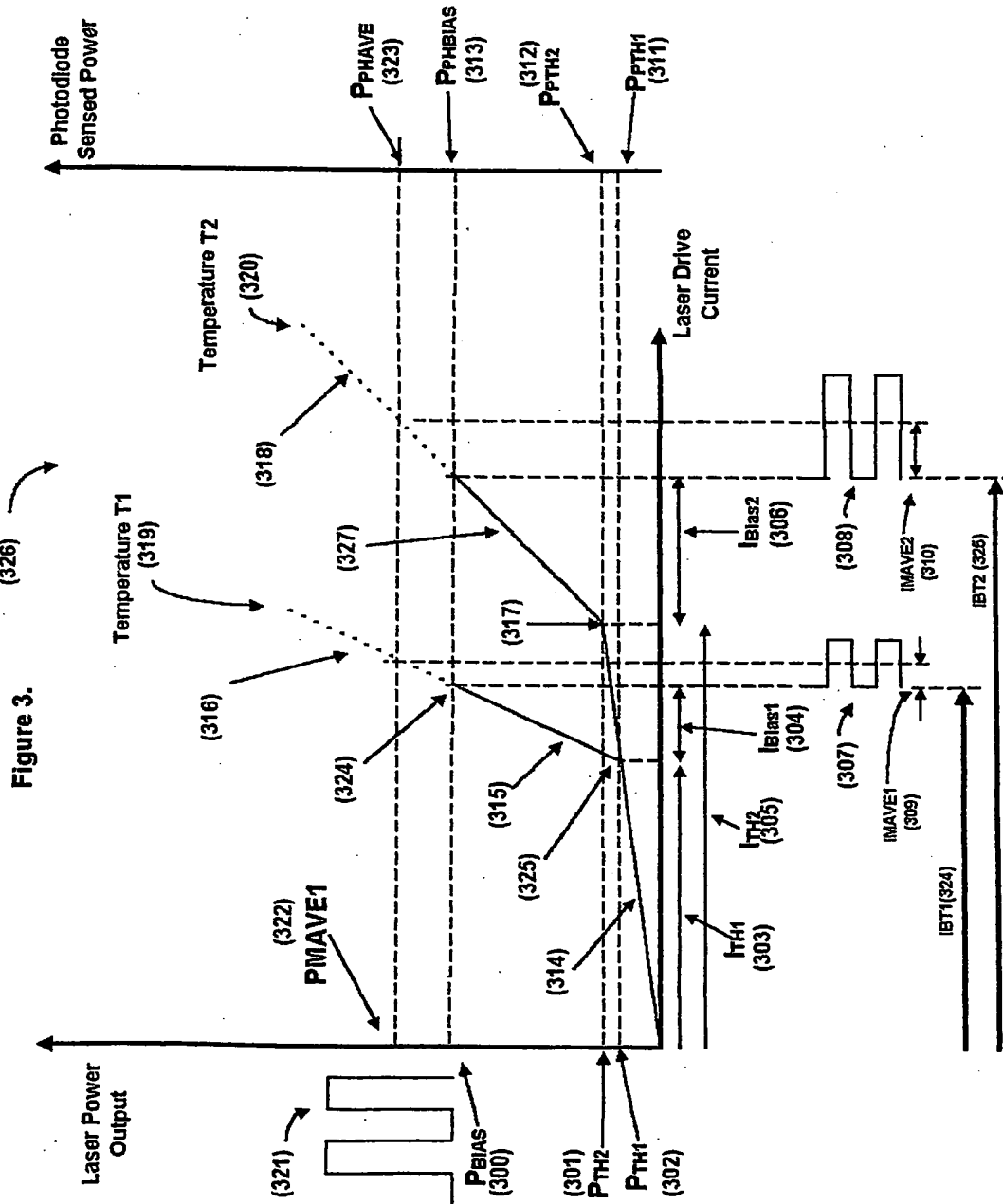


Figure 2.  
Laser Power Sensing Timing Diagram





# INTERNATIONAL SEARCH REPORT

International application No.

PCT/US03/01032

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) : G06K 7/10; H01S 3/13, 3/00

US CL : 235/454, 455; 372/29, 38

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 235/454, 455; 372/29, 38

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y — P	US 6,414,974 B (RUSSELL et al) 02 July 2002 (02.07.2002), see entire document.	1-5
Y	US 5,625,616 A (KOIKE et al) 29 April 1997 (29.04.1997), see entire document.	1-5
Y	US 5,334,826 A (SATO et al) 02 August 1994 (02.08.1994), see entire document.	1-5
Y	US 4,995,105 A (WECHSLER et al) 19 February 1991 (19.02.1991), see entire document.	1-5
A	US 5,502,298 A (GELLER et al) 26 March 1996 (26.03.1996), see entire document.	1-5
A	US 5,982,794 A (TAMURA et al) 09 November 1999 (09.11.1999), see entire document.	1-5

☐ Further documents are listed in the continuation of Box C.

☐ See patent family annex.

\* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier application or patent published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T"

later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X"

document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y"

document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&"

document member of the same patent family

Date of the actual completion of the international search

12 March 2003 (12.03.2003)

Date of mailing of the international search report

18 JUN 2003

Name and mailing address of the ISA/US

Commissioner of Patents and Trademarks

Box PCT

Washington, D.C. 20231

Facsimile No. (703)305-3230

Authorized officer

April A. Nowlin

Telephone No. (703) 605-1219

*Donna P. Vega*  
Deborah P. Vega

Paralegal Specialist

Technology Center 2800  
(703) 308-3078